RADIOMETRIC MEASURING DEVICE

The invention relates to a radiometric measuring device. By means of radiometric measuring devices, physical variables, e.g. a fill level or a density of a medium, are measurable.

Radiometric measuring devices are usually always applied, when conventional measuring devices can not be used at the measuring site, because of especially rough conditions. Very frequently, e.g. extremely high temperatures and pressures reign at the measuring site, or chemically and/or mechanically very aggressive, environmental influences are present, which make the use of other measuring methods impossible.

In radiometric measurement technology, a radioactive source, e.g. a Co 60 or a Cs 137 preparation, is placed in a radiation protection container and brought to a measuring location, e.g. to a container filled with a filling substance. Such a container can be e.g. a tank, a pipe, a conveyor belt or any other possible form of containment.

The radiation protection container has a window, through which the radiation emitted by the source positioned for the measurement is radiated out, through a wall of the radiation protection container.

Usually, a radiating direction is selected, such that the radiation passes through that region of the container which is to be registered for measurements. On the oppositely lying side, emerging radiation intensity changed by a fill level, or density, change is quantitatively registered with a detector. The emerging radiation intensity is dependent on the geometric arrangement and on the absorption. The latter

is, in the case of fill level measurements, dependent on the amount of filling substance in the container, and, in the case of density measurements, on the density of the filling substance. As a result, the emerging radiation intensity is
5   a measure for the current fill level, or the current density, of the filling substance in the container.

Suitable as detectors are e.g. a scintillation detector having a scintillator, e.g. a rod-shaped scintillation probe,
10 and a photomultiplier. The scintillation probe is, in principle, a Plexiglas rod, which is optically very pure. Under the influence of gamma radiation, light flashes are emitted by the scintillation material. These are registered by the photomultiplier and converted into electrical pulses.
15 A pulse rate, with which the pulses occur, depends on the radiation intensity and is, therefore, a measure for the physical variable to be measured, e.g. the fill level or the density. Scintillators and photomultipliers are usually assembled into a protective tube e.g. of a high grade steel,
20 e.g. a high grade, stainless steel.

The detector includes, as a rule, an electronics, which makes available to a superordinated unit an output signal corresponding to the pulse rate. The electronics includes,
25 usually, a control unit and a counter. The electrical pulses are counted and a count rate is derived, on the basis of which the physical variable to be measured is determinable.

Additionally, preferably a status of the detector is checked.
30 The status involves, in the simplest case, an indication concerning whether the detector is working properly or not. Depending on the status, as required, a malfunction report and/or an alarm is triggered.

For transmitting the output signal and status of a detector, as a rule, two lines are provided between the detector and the superordinated unit.

5   An effective length of the detectors determines the measurable range of the container and depends on the required measurement height and the mounting opportunities. Detectors are obtainable, at this time, in lengths of about 400 mm to about 2000 mm. If a length of about 2000 mm is not
10 sufficient, then two or more detectors can be connected to a radiometric measuring device.

A feature of conventional measuring devices is that each detector has its own electronics. For transmitting the
15 output signals and status of each detector, at least two lines are run from each detector to the superordinated unit. The output signals of individual detectors are combined in the superordinated unit to a sum signal, which reflects the total rate of the registered pulses.
20

In the application of two or more detectors, the required technical effort rises in proportion to the number of detectors. For each detector, its own electronics is to be provided, with a counter and a control unit, the status of
25 each detector must be separately checked, and each detector is to be connected with the superordinated unit by means of two lines. The superordinated unit must then check the status of each detector and combine the individual output signals to a measurement signal.
30

Each additional line increases the costs. Especially, when the detectors are placed in explosion-endangered areas, the costs for additional lines are considerable.

It is an object of the invention to provide a radiometric measuring device having two or more detectors, which can be installed and operated cost-favorably.

5   To this end, the invention involves a radiometric measuring device for mounting at a container fillable with a filling substance, including
     - a radioactive source, which, in operation, sends radioactive radiation through the container,
10   - at least two detectors,
     --which serve for registering radiation passing through the container and for producing an electrical pulse rate corresponding to the registered radiation,
     - offset generators, which superimpose on the pulse rate of
15   each detector an offset representing a status of such detector, and
     - a collector line,
     --to which each detector feeds an output signal corresponding to the superimposing of its pulse rate and its offset,
20   --which feeds to a superordinated unit a sum signal corresponding to the superimposing of the output signals,
     ---with the superordinated unit deriving, on the basis of the sum signal, a measurement signal and/or a status of the measuring device.
25
     Further, the invention involves a radiometric measuring device for mounting at a container fillable with a filling substance, including
     - a radioactive source, which, in operation, sends
30   radioactive radiation through the container,
     - at least two detectors,
     --which serve for registering radiation passing through the container and for producing an electrical pulse rate corresponding to the registered radiation,

- offset generators, which superimpose on the pulse rate of
each detector a detector-specific offset, and
- turn-off switches, which serve for suppressing transmission
of pulse rate and offset, when a detector malfunctions,
5   - a collector line,
--to which each properly working detector feeds an output
signal corresponding to the superimposing of its pulse
rate and its offset, and
--which feeds to a superordinated unit a sum signal
10   corresponding to the superimposing of the output signals,
---with the superordinated unit deriving, on the basis of the
sum signal, a measurement signal and/or a status of the
measuring device.

15 According to an embodiment of the above-defined, radiometric
measuring device, a series of detectors is provided, and the
collector line begins at a first detector of the series,
leads from there from one detector to the detector
neighboring such, and from the last detector to the
20 superordinated unit.

In a further embodiment, each detector comprises a
scintillator and a photomultiplier appended thereto.

25 According to a further development of the last-mentioned,
radiometric measuring device, the offset-generators send
periodic reference light flashes through the scintillator via
a light conductor.

30 In a further embodiment, the superordinated unit is
integrated in the last detector of the series.

The invention further resides in a method for measuring a
physical variable with one of the above-defined, radiometric

measuring devices, wherein
- a desired value for an offset is assigned to each detector,
  the offset generators of the detectors generate the desired
  value when the detector is working properly, and the
5 desired value is greater than a sum of the maximum expected
  pulse rates for the detectors, and wherein
- the superordinated unit determines a total count rate on
  the basis of the sum signal,
- forms the difference between this total count rate and a
10 count rate corresponding to the sum of the desired values
  of the offsets,
- recognizes that an error is present, when the difference is
  negative, and
- in the case of positive difference, derives a measurement
15 signal.

According to an embodiment of the method, in the case of a
negative difference, it is determined on the basis of the
amount of the difference, which of the detectors is
20 malfunctioning.

Further, the invention resides in a radiometric measuring
device for mounting at a container fillable with a filling
substance, comprising
25 - a radioactive source, which, during operation, sends
  radioactive radiation through the container,
- first and second detectors,
--which serve for registering radiation passing through the
  container and for producing an electric pulse rate
30 corresponding to the registered radiation,
- an offset-generator, which superimposes on the pulse rate
  of the first detector an offset reflecting a status of the
  first detector, and,
- integrated in the second detector, a superordinated unit,

--with which the first detector is connected via a connecting
    line,

---via which the first detector feeds an output signal
    corresponding to the superpositioning of the pulse rate

5   and the offset,

--to which the pulse rate and a status of the second detector
    are fed, and

--which, on the basis of the incoming signals, derives a
    measurement signal and/or a status of the measuring

10   device.

Further, the invention resides in a radiometric measuring
device for mounting at a container fillable with a filling
substance, comprising

15 - a radioactive source, which, during operation, sends
    radioactive radiation through the container,

- first and second detectors,

--which serve for registering radiation passing through the
    container and for producing an electric pulse rate

20   corresponding to the registered radiation and for
    transmitting an output signal corresponding to the pulse
    rate to a superordinated unit integrated in the second
    detector,

- wherein the source has a strength, in the case of which,

25   for each detector, always a minimum pulse rate greater than
    zero is to be expected,

- wherein, in each detector, a turn-off switch is provided,
    which suppresses transmission of the output signal to the
    superordinated unit, when the detector is malfunctioning,

30   and

- wherein the superordinated unit derives a measurement
    signal and/or a status of the measuring device on the basis
    of the output signals.

An advantage of the invention is that the detectors are only connected by a single line, the collector line, or the connecting line, as the case may be, via which both the status information and the measurement information are
5   transmitted, because a single output signal is produced, which contains both pieces of information. This happens by superimposing a status-dependent offset on the pulse rate, or by superimposing on the pulse rate a detector-specific offset dependent on status, or this does not happen.
10

The invention and further advantages will now be explained in greater detail on the basis of the figures of the drawing, in which seven examples of embodiments are presented; equal parts are provided in the figures with equal reference
15   characters. The figures show as follows:

Fig. 1   schematically, a container-mounted, radiometric, measuring device having two detectors;

20   Fig. 2   schematically, the construction of a detector;

Fig. 3   schematically, a superimposing of pulse rate and offset;

25   Fig. 4   a signal corresponding to the superimposing of Fig. 3;

Fig. 5   schematically, the construction of a measuring device having three detectors, wherein, on the
30   pulse rate of each detector is superimposed an offset dependent on the status of the detector;

Fig. 6   schematically, the construction of a measuring device having three detectors, wherein a detector-

specific offset is superimposed on the pulse rate of each detector;

Fig. 7   schematically, the construction of a detector, wherein, depending on the status of the detector, an offset generator for producing a detector-specific offset, or a turn-off switch, is used;

Fig. 8   schematically, the construction of a measuring device having two detectors, wherein at least one detector has an offset generator, which superimposes on the pulse rate of the detector an offset depending on the status of the same;

Fig. 9   schematically, the construction of a measuring device having two detectors, each of which has a turn-off switch, which suppresses transmission of the pulse rate when the relevant detector is not working properly; and

Fig. 10   the construction of a detector having an offset generator, which feeds reference light flashes to the scintillator.

Fig. 1 shows, schematically, a measuring arrangement with a radiometric measuring device. The measuring arrangement includes a container 3 fillable with a filling substance 1. The radiometric measuring device is mounted at the container 3 and serves for registering a physical variable, e.g. a fill level of the filling substance 1 in the container 3, or a density of the filling substance 1.

To this end, the radiometric measuring device includes a radioactive source 5, which sends radioactive radiation

through the container 3 during operation. Source 5 includes
e.g. a radiation protection container, in which is housed a
radioactive preparation, e.g. a Co 60 or Cs 137 preparation.
The radiation protection container has a window, through
5 which the radiation emerges at a spreading angle α and passes
through the container 3.

The measuring device further includes at least one detector
D, which serves for registering the radiation passing through
10 the container 3 and for producing an electric pulse rate N
corresponding to the registered radiation. Depending on
application, a plurality of detectors D_i can be connected one
after the other, in order to cover a sufficiently large
range, in which radiation can be registered. In the example
15 of an embodiment shown in Fig. 1, two detectors D_1 and D_2 are
provided.

Fig. 2 shows a simplified construction of a detector D_i. In
this case, a scintillation detector is shown, with a
20 scintillator 7, here a rod-shaped scintillation probe, and a
photomultiplier 9 appended thereto. Scintillator 7 and
photomultiplier 9 are located in a protective tube 11 shown
in Fig. 1, for instance a protective tube of high-grade
steel, for example a stainless, high-grade steel. Tube 11 is
25 mounted on an outer wall of container 3. The outer wall lies
opposite to the source 5. The rod-shaped scintillation probe
is, in principle, a rod of Plexiglas material of optically
very high purity. Radiation impinging on the scintillator 7
produces light flashes in the scintillation material. These
30 are registered by the photomultiplier 9 and converted into
electrical pulses n.

Each detector D_i includes an electronics 13, which registers
electrical pulses n produced by the photomultiplier 9 and

produces a pulse rate N corresponding to the registered radiation.

5   The electronics 13 includes, preferably, a counter 15 and a microcontroller 17 connected thereto. The counter 15 counts the incoming electric pulses n and the microcontroller 17 determines, on the basis of the counted pulses n, a pulse rate N.

10   According to a first form of embodiment, each detector D_i has, additionally, an offset-generator 19, which produces an offset O_i corresponding to a status of the particular detector D_i. The offset generators 19 are, preferably, and as shown in Fig. 2, integrated into the microcontroller 17. Suitable as
15   offset generator 19 is e.g. a pulse generator, which produces electrical pulses K with a frequency corresponding to the offset O_i. The offset O_i is superimposed on the pulse rate N_i of the relevant detector D_i. Fig. 3 shows such a superimposing schematically. In such case, the pulses K
20   produced by the offset generator 19 are added to the electrical pulses n registered by the photomultiplier 9. An output signal corresponding to the superimposing is shown in Fig. 4, where the pulses K of the offset generator 19 are shown as rectangular pulses. The pulses n of the
25   photomultiplier 9 are likewise shown as rectangular pulses. For distinguishing between the two different kinds of pulses, dashed lines have been used to show the pulses n of the photomultiplier 9.

30   The output signal is generated in the microcontroller 17 and is available via an output stage 20 of the microcontroller 17.

A collector line 21 is provided, to which each detector D_i

feeds its output signal corresponding to the superimposing of its pulse rate N_i and its offset O_i.

5   The collector line 21 leads from one detector D_i to the next, neighboring detector D_{i+1}. Fig. 5 shows an example of an embodiment having a series of three detectors D_1, D_2 and D_3 connected one after the other. The connecting line 21 begins at the first detector D_1 of the series. It leads from each detector D_i to the neighboring detector D_{i+1} of the series and
10   ends at the last detector of the series. In Fig. 5, this is detector D_3. From the last detector D_3, it leads to a superordinated unit 23.

     In the collector line 21, the output signals of the
15   individual detectors D_i superimpose to form a sum signal S, which corresponds to the sum of the individual output signals.

     The superordinated unit 23 derives, on the basis of the sum
20   signal S, a measurement signal M and/or a status signal of the measuring device. To accomplish this, various methods can be used.

     A first method will now be explained in greater detail on the
25   basis of the example of an embodiment shown in Fig. 5 as follows. In such case, a desired value O_{si} for the offset O_i is assigned to each detector D_i. The desired values O_{si} are to be so selected, that they are greater than a sum of the maximum pulse rates N_i^{max} to be expected for the respective
30   detectors D_i.

$$O_{si} > \Sigma_i\, N_i^{max}$$

     If the maximum expected pulse rate N_i^{max} of each detector D_i

is, for example, smaller than 20 pulses n per interval of time, then the desired values O_{si} in the example of Fig. 5 are to be chosen to be greater than 60 pulses K per interval of time.

In the simplest case, the offset generators 19 of the detectors D_i are made to produce a offset O_i which corresponds to the desired value O_{si}, when the particular detector D_i is working properly, and no offset, i.e. an offset of 0 pulses K per interval of time, when the detector D_i is not working properly.

The superordinated unit 23 contains a counter 25 and an evaluating unit 27 connected thereto. The counter 25 counts the incoming pulses n_i, K_i. On the basis of the sum signal, a total count rate G is determined. The total count rate G is equal to the sum of the individual pulse rates N_i of the individual detectors D_i and the individual offsets O_i.

The following holds:

$$G = \Sigma_i(N_i + O_i)$$

In a next step, the evaluating unit 27 of the superordinated unit 23 forms a difference between this total count rate G and a count rate corresponding to the sum of the desired values O_{si} of the offsets O_i. For this purpose, there is connected to the evaluating unit 27 a memory 28, in which the desired values O_{si} of the offsets O_i are stored.

The following holds:

$$D = G - \Sigma_i O_{si}$$

When all detectors are working properly, this difference is positive and equal to the sum of the pulse rates N_i of the individual detectors D_i.

5   If at least one detector D_i is not working properly, the difference D is negative. A negative difference D means that an error is present. At least one of the detectors is not working properly.

10   The evaluating unit 27 determines, whether the difference D is positive or negative. It recognizes that an error is present, when the difference D is negative.

Additionally, it is possible, in the case of the presence of
15   a negative difference D, i.e. an error, on the basis of the magnitude, or absolute value, $|D|$ of the difference D, to determine, which of the detectors D_i is malfunctioning. This makes a search for the error easier, following recognition of the error, as well as facilitating the eliminating of the
20   error.

For this, for instance in the example of an embodiment presented with respect to Fig. 5, all desired values O_{si} of the offset O_i are so selected, that they differ from one
25   another, and the difference of each pair of desired values O_{si} is, in each case, greater than the sum of the maximum pulse rates $N_i$max to be expected for the considered detectors D_i; i.e., the following holds:

30     $O_{si} \neq O_{sj}$, when $i \neq j$;

$|O_{si} - O_{sj}| > \Sigma_i \, N_i^{max}$

$O_{si} > \Sigma_i \, N_i^{max}$.

If, as given above in terms of an example, $N_i^{max} < 20$, then, for example, the desired values can be selected as follows: $O_{s1} = 100$, $O_{s2} = 200$ and $O_{s3} = 300$.

5   If a single detector D_i is not operating properly, then the following holds for the magnitude $|D|$ of the difference D:

$$|D| = |\Sigma_i N_i - O_{si}| \quad \text{and, thus,}$$

10    $$O_{si} - \Sigma_i N_i^{max} < |D| < O_{si}.$$

If detector D_1 is not working properly, then the magnitude $|D|$ of the difference D lies, as a result, between 40 and 100. If detector D_2 is not working properly, then the magnitude $|D|$ 15   of the difference D lies, as a result, between 140 and 200. If detector D_3 is not working properly, then the magnitude $|D|$ of the difference D lies, as a result, between 240 and 300.

Thus, on the basis of the magnitude $|D|$ of the difference D, 20   it is possible, unequivocally, to determine which D_i is not working properly. The assigning of the magnitude $|D|$ of the difference D to the affected detector D_i assumes, however, that only a single detector D_i is not working properly.

25   If one would want also to determine in the case of two detectors D_i and D_j not working properly, which detectors D_i, D_j these are, then the following must additionally hold for the desired values O_{si}, O_{sj} of the offsets O_i, O_j of every possible affected detector pair D_i, D_j:
30

$$O_{si} + O_{sj} \notin [O_{sk} - \Sigma_i N_i^{max} ; O_{sk} + \Sigma_i N_i^{max}]$$

For instance, in the case of the above example, the desired

values for the first, second and third detectors D_1, D_2, D_3 can be, for example, $O_{s1} = 100$, $O_{s2} = 500$ and $O_{s3} = 1000$, respectively.

5   If only one detector D_i is not working properly, then the following holds for the magnitude $|D|$ of the difference D:

$$|D| = |\Sigma_i \, N_i - O_{si}| , \text{ and, thus,}$$

10   $$O_{si} - \Sigma_i \, N_i^{max} < |D| < O_{si}.$$

If detector D_1 is not working properly, then the magnitude $|D|$ of the difference D lies between 40 and 100. If detector D_2 is not working properly, then the magnitude $|D|$ of the 15   difference D lies between 440 and 500. If detector D3 is not working properly, then the magnitude $|D|$ of the difference D lies between 940 and 1000.

If the detectors D_i and D_j are not working properly, then the 20   following holds for the magnitude $|D|$ of the difference D:

$$|D| = |\Sigma_i \, N_i - O_{sj} - O_{si}| , \text{ and, thus,}$$

$$O_{si} + O_{sj} - \Sigma_i \, N_i^{max} < |D| < O_{sj} + O_{si}.$$
25

If the detectors D_1 and D_2 are not working properly, then the magnitude $|D|$ of the difference D lies between 540 and 600. If the detectors D_1 and D_3 are not working properly, then the magnitude $|D|$ of the difference D lies between 1040 and 1100. 30   If the detectors D_2 and D_3 are not working properly, then the magnitude $|D|$ of the difference D lies between 1440 and 1500.

If none of the detectors D_1, D_2 and D_3 is working properly,

then the magnitude |D| of the difference D lies between 1540 and 1600.   Thus, in the defined example of an embodiment, also this last case can be recognized on the basis of the magnitude |D| of the difference D.

5

If more than three detectors are employed, then the method can be correspondingly expanded.

The superordinated unit 23 recognizes, on the basis of the
10   difference D, the presence of an error and derives therefrom the status of the measuring device.   In the simplest case, the status contains the information that all detectors D_i are working properly, or at least one of these is not. Additionally, the status can, in the case of an error,
15   contain the information as to which of the one or more detectors D_i is not working properly.

In the presence of an error, the superordinated unit 23 produces an output signal reflecting the status, which is
20   fed, for example, to a measuring device electronics 29, or to a process control location.   The superordinated unit can also issue an error report and/or trigger an alarm.

If no error is present, then the difference D is positive.
25   The superordinated unit recognizes this and produces a measurement signal M on the basis of the sum signal.   In the simplest case, the measurement signal corresponds to the difference D.   When all detectors are working properly, this difference is positive and equal to the sum of the individual
30   pulse rates N_i of the individual detectors D_i:

$$D = G - \Sigma_i O_{si} = \Sigma_i N_i$$

On the basis of this measurement signal, the physical

variable to be measured, e.g. a fill level or a density of the filling substance, is determined. This can occur in conventional manner either by means of a measuring device electronics 29 integrated in the superordinated unit 23 or in
5   a remotely located, evaluating unit 31.

If all detectors D_i are working properly, the superordinated unit 23 can likewise issue an output signal reflecting the status. In this way, also the error-free working of the
10   detectors D_i can be indicated to, for example, the measuring device electronics 29, the evaluating unit 31 or to some other location, e.g. a process control location.

The superordinated unit 23 can be located in the last
15   detector of a series; it can, however, also be arranged separately. The same holds for the measuring device electronics 29.

An advantage of the invention is that, due to the
20   superimposing of the pulse rates N_i and the offsets O_i, and their transport together in the collector line 21, only a single connecting line, namely the collector line 21, is required for transmitting both the actual measurement information and also the status information. This reduces
25   the required wiring effort considerably. Especially in safety-relevant regions, in which radiometric measuring devices are usually applied, e.g. in regions with increased danger of explosion, there are high safety demands placed on connecting lines, with which, as a rule, are associated
30   increased procurement and installation costs. These costs are markedly reduced by the radiometric measuring devices of the invention. The collector line 21 can be a very simple connection, e.g. a light wave conductor, e.g. an optical fiber, or a copper line. Likewise, it is possible to replace

the collector line 21 with a radio connection.

The transmission can be done in very simple manner. Especially, no transmission protocol is needed. The
5 transmission of the output signals of the individual detectors D_i can, in fact, with appropriate calibration, be accomplished via any kind of pulse output directed to a corresponding pulse input of the superordinated unit 23.

10 Fig. 6 shows a further example of an embodiment of a radiometric measuring device of the invention. Since most of the features of this embodiment are the same as in the above-described example of an embodiment, only differences will be explained in more detail in the following.
15

Also here, detectors D_i are provided, which serve for registering radiation passing through the container 3 and for producing an electrical pulse rate N_i corresponding to the registered radiation. Each detector D_i includes an offset
20 generator 19, which superimposes on the pulse rate N_i of the pertinent detector D_i a detector-specific offset O_{di}. In contrast to the above example of an embodiment, here the offsets O_{di} are detector-specific and independent of the status of the pertinent detector D_i.
25

Each detector D_i includes a turn-off switch 33, which serves for suppressing transmission of the pulse rate N_i and the offset O_{di}, when the detector D_i is malfunctioning. Turn-off switch 33 is, for example, a simple switch, which interrupts
30 the connection of the pertinent detector D_i to the collector line 21. Turn-off 33 switch can, however, also be integrated in the output stage 20 of the microcontroller 17.

During operation, therefore, only every properly working

detector D_i feeds an output signal, corresponding to the superimposing of the pertinent pulse rate N_i and the pertinent offset O_{di}, to the collector line 21. Non-properly working detectors D_i, in contrast, issue no output signal.

5

The collector line 21 feeds, as also the case in the above-described example of an embodiment, a sum signal, corresponding to the superimposing of the output signals, to the superordinated unit 23. This derives, as already described in connection with the above example of an embodiment, a measurement signal and/or a status of the measuring device on the basis of the sum signal.

With appropriate choice of the detector-specific offsets O_{di}, it is possible here, exactly as in the case of the example of an embodiment described above, to recognize, which of one or more detectors is not working properly. Additionally, a remainder count rate R can be determined, which is equal to the sum of the count rates N_i of the properly-working detectors D_i.

Such is equal to the difference between the total count rate G and the sum of the offsets O_{di} of the properly working detectors D_i. If, for example, the detector D_x is not working properly, then the following holds:

$$R = G - \Sigma_{i, i \neq x}\, O_{di}$$

From this, as required, helpful additional information can be derived. As an example, only a fill level measurement with two detectors is treated, such as is illustrated in Fig. 1. If one of the detectors D_1, D_2 fails, then it is possible, on the basis of the count rate N_i of the remaining detector, to determine whether filling substance 1 is located in the

region of the container 3 covered by the remaining detector. This rudimentary fill level information can be used e.g. for safety-directed control of a filling or emptying of the container 3. For instance, an overfilling or complete 5 emptying of the container can be prevented.

Alternatively to the form of embodiment presented in Fig. 6, the detectors D_i can also be so constructed, that a turn-off switch 35 only suppresses the superimposing of the detector-10 specific offset O_{di}, when the relevant detector D_i is not working properly. This is shown in Fig. 7. If the detector D_i is not working properly, the addition of the offset O_{di} is suppressed by the turn-off switch 35. This is represented in Fig. 7 by the feeding of the signals of offset generator 19 15 and turn-off switch 35 through a switch V. This combination of offset generator 19 and turn-off switch 35 forms, in effect, an offset generator, which issues a status-dependent offset. The sum signal is used in this case exactly as in the case of the example of an embodiment explained on the 20 basis of Fig. 5.

Fig. 8 presents an example of an embodiment, wherein the measuring device has two detectors, namely a first detector D_1 and a second detector D_2. The measuring device is mounted at 25 the container 3 fillable with the filling substance 1. The radioactive source 5 sends radioactive radiation through the container 3 during operation. The first and second detectors D_1 and D_2 serve for registering radiation passing through the container 3 and for producing electric pulse rates N_1, N_2 30 corresponding to the registered radiation.

The first detector D_1 has an offset generator, which superimposes on the pulse rate N_1 of the first detector D_1 an offset O_1 reflecting the status of the first detector D_1.

This is accomplished, for example, exactly as in the case of the example of an embodiment described with respect to Fig. 5.

5   Also here, a superordinated unit 23 is provided, integrated in the second detector D_2. The first detector D_1 is connected via a connecting line 37 with the superordinated unit 23, via which the first detector D_1 feeds an output signal corresponding to the superimposing of the pulse rate N_1 and
10   the offset O_1. The connecting line 37 is connected for this purpose to a first input 39 of the superordinated unit 23.

Additionally fed to the superordinated unit 23 are the pulse rate N_2 and the status of the second detector D_2.

15
To this end, the second detector D_2 can be equipped, exactly as in the case of the first detector D_1, with an offset generator 19, which superimposes on the pulse rate N_2 an offset O_2 reflecting the status of the second detector D_2. An
20   output signal corresponding to this superimposing lies then on a second input 41 of the superordinated unit 23.

Alternatively, the superordinated unit 23 can register the status information directly via a third input 43. The second
25   detector then, in the case of this variant of embodiment, does not have an offset generator 19. Thus, Fig. 8 shows both the offset generator 19 of the second detector D_2 and the alternatively provided, third input 43.

30   The superordinated unit derives, on the basis of the incoming signals, a measurement signal and/or a status of the measuring device.

This happens, analogously to the examples of embodiments

described above, by assigning to the offsets O_1 and, as required, O_2, desired values O_{s1}, O_{s2}, which the respective offset O_1, O_2 assumes, when the associated detector D_1, D_2 is working properly. If a detector D_1, D_2 is not working
5   properly, then, for example, no offset is superimposed.

Since the superordinated unit 23 is integrated in the second detector D_2, the information of the detectors D_1 and D_2 can be processed separately via the inputs 37, 39, and, as required,
10   41, without other lines running outside of the detectors being required in addition to the connecting line 37.

This offers the advantage that the desired values O_{s1} and, as required, O_{s2} must only be greater than the maximum pulse rate
15   $N_i max$ expected for the pertinent detectors D_1, D_2, but, by all means, can be smaller than the sum of the maximum expected pulse rate $N_1^{max} + N_2^{max}$. This improves the accuracy of measurement.

20   On the basis of the output signal of the first detector D_1, the superordinated unit 23 determines a count rate Z_1, which is equal to the sum of the pulse rate N_1 and the offset O_1. Then, the difference between this count rate Z_1 and the desired value O_{s1} for the offset O_1 of the first detector is
25   formed. If the difference is positive, then detector D_1 is working properly and the magnitude of the difference is equal to the pulse rate N_1 of the first detector D_1. If the difference is negative, then the superordinated unit 23 recognizes that detector D_1 is not working properly.
30
In the case of the variant of the embodiment, in which the second detector D_2 is likewise equipped with an offset generator 19, the second detector D_2 is used in an analogous manner, i.e. the superordinated unit 23 determines, on the

basis of the output signal of the second detector D_2, a count rate Z_2, which equals the sum of the pulse rate N_2 and the offset O_2. Then, the difference between this count rate Z_2 and the desired value O_{s2} for the offset O_2 of the second

5 detector D_2 is formed. If the difference is positive, then detector D_2 is working properly and the magnitude of the difference is equal to the pulse rate N_2 of the second detector D_2. If the difference is negative, then the superordinated unit 23 recognizes that the detector D_2 is not

10 working properly.

In the case of the alternative variant of the embodiment, in which the status information is separately transmitted, the superordinated unit recognizes directly on the basis of the

15 signal lying on the third input 43, whether the second detector D_2 is working properly. Further, it determines, on the basis of the output signal of the second detector D_2 incoming on the second input 41, a count rate Z_2, which equals the pulse rate N_2 of the second detector D_2.

20

In the case of both variants, the status of the first and second detectors then is present in the superordinated unit 23.

25 If both detectors D_1, D_2 are working properly, then the pulse rates N_1 and N_2 are present in the superordinated unit 23. Simple addition of the pulse rates N_1 and N_2 leads to a measurement signal, which corresponds to the radiation registered by the two detectors D_1 and D_2. Additionally, the

30 measurement information of each individual detector D_1, D_2 is available on the basis of the individual pulse rates N_1, N_2. If only one of the detectors D_1 or D_2 is working properly, this additional information can be separately used, as already explained above.

Fig. 9 shows a further example of an embodiment of a measuring device of the invention. Its construction corresponds, for the most part, to the example of an
5   embodiment presented in Fig. 8. Therefore, only the differences will be explained in detail in the following.

In the case of the example of an embodiment presented in Fig. 9, the source 5 has a strength, at which a minimum pulse rate
10   N_i^{min} greater than zero is always to be expected for each detector D_1, D_2.

The first detector D_1 is connected via the connecting line 37 to the first input 39 of the superordinated unit 23
15   integrated in the second detector D_2, while the second detector D_2 is directly connected to its second input 41. In contrast to the example of an embodiment illustrated in Fig. 8, no offset generators 19 and no third input 43 are provided.
20

Instead, in each detector D_1, D_2, a turn-off switch 45 is provided, which suppresses the transmission to the superordinated unit of an output signal corresponding to the pulse rate N_1, N_2 of the pertinent detector D_1, D_2, when such
25   detector D_1, D_2 is malfunctioning.

The signals of the detectors D_1 and D_2 fed to the superordinated unit 23 thus correspond to the pulse rates N_1, N_2 of the detectors D_1, D_2, when such are working properly.
30

The superordinated unit 23 has, preferably, a first counter, which counts the pluses n_1 incoming at the first input 39 and a second counter, which counts the pulses n_2 incoming at the second input 41, and determines the count rates Z_1, Z_2 of the

incoming pulses n_1, n_2. If a count rate Z_1, Z_2 is zero pulses per time interval, then the superordinated unit 23 recognizes that the associated detector D_1, D_2 is not working properly. From this, the status of the measuring device is derived, and

5   a corresponding status information is made available. The status information contains the statement that both detectors D_1 and D_2 are working properly, when both count rates Z_1 and Z_2 are different from zero. For the case that one or both count rates Z_1, Z_2 equal(s) zero, it contains the information that

10   the measuring device is not working properly. Additionally, the status information can contain data concerning which of the detectors D_1, D_2 is not working properly, or whether both of the detectors D_1, D_2 are not working properly.

15   The status information is provided via an output 47 of the superordinated unit 23. Output 47 is preferably the only output of the second detector, as well as the only output of the measuring device. On the basis of the status information, an alarm can, for example, be triggered.

20

If both count rates Z_1 and Z_2 are different from zero, then both detectors D_1 and D_2 are working properly, and the superordinated unit 23 derives a measurement signal. This is based on the sum of the count rates, $Z_1 + Z_2$, which, in this

25   case, is equal to the sum of the pulse rates $N_1 + N_2$ of the detectors D_1 and D_2. The measurement signal can, in such case, be a signal, which reflects the sum of the pulse rates $N_1 + N_2$. The measurement signal is then, for example, fed to a measuring device electronics 29 or to a separate evaluating

30   unit 31, which determines, on the basis of the measurement signal, the variable to be measured with the measuring device, e.g. a fill level or a density. The measuring device electronics 29 is, for example, likewise arranged in the second detector D_2.

Alternatively, an evaluation and/or processing of the pulse rates $N_1 + N_2$ can also occur in the superordinated unit 23.

5 Status and/or measurement signal is/are available via the output 47.

In the case of all measuring devices of the invention, a single collector line, or a single connecting line, suffices
10 for transmitting both the status and also the actual measurement information.

Each detector D_i can, naturally, only transmit its status to the superordinated unit 23, when the status has already
15 earlier been determined. In the technology of measurements, a series of methods for control and/or monitoring of the proper functioning of detectors are known.

An example, in this connection, is the control and/or
20 monitoring of the energy, or power, supply of the detectors or individual detector components.

Further, it is possible, in the case of the described detectors D_i, to check the optical coupling between the
25 scintillator 7 and the photomultiplier 11.

To this end, e.g. reference light flashes are sent continuously through the scintillator 7 via the light conductor 49. Independently of whether the scintillator 7 is
30 subjected to gamma radiation, or not, reference pulses must, due to the reference light flashes, be present on the output of the photomultiplier 11. If this is not the case, then the pertinent detector D_i is not working properly.

In the case of measuring devices of the invention, in which
the detectors D_i include offset-generators 19, which
superimpose on the pulse rate N_i an offset O_i dependent on the
status of the pertinent detector D_i, the status determination
5   occurs, preferably, in the manner illustrated in Fig. 10, in
that the offset generators 19 of the detectors D_i are
connected to the scintillator 7 via light conductors 49.
During operation, the offset generators 19 periodically
produce reference light flashes I and send these through the
10   scintillator 7.

Preferably, the frequency f_i, with which the reference light
flashes are emitted, equals the initially described, desired
value O_{si} for the offset O_i of the pertinent detector D_i. If
15   the detector D_i is working properly, then, on the output,
there is a signal which corresponds to the sum of the pulse
rate N_i and the desired value O_{si}. If a disturbance is
present, markedly fewer pulses are detected. If the pulse
rate of the detected pulses falls beneath the desired value
20   O_{si}, then this leads to a negative difference D.

An advantage of the invention is that, in the case of all
radiometric measuring devices of the invention, only a single
connection, namely the connector line 21, or the connecting
25   line 37, as the case may be, is needed, in order to transmit
both the actual measurement information as well as also the
status information. This reduces the required wiring effort
considerably. Especially in safety-relevant areas, in which
radiometric measuring devices are usually applied, e.g. in
30   areas with increased danger of explosion, there are high
safety demands on connecting lines, with which are
associated, as a rule, increased procurement and installation
costs. These costs are markedly reduced by the radiometric
measuring devices of the invention. This can be a very

simple connection, e.g. a light wave conductor or a copper line.   Likewise is it possible to embody the connection as a radio connection.

5   The transmission can be done in very simple manner. Especially, no transmission protocol is needed.   The transmission of the output signals of the individual detectors D_i can, in fact, occur, in the case of appropriate calibration, via every kind of pulse output to a
10   corresponding pulse input of the superordinated unit 23.